

Modelling and design of a physical system to simulate the cardiovascular systemic arterial load using a windkessel model





Outline

- Introduction
 - Objectives
 - Model Selection
- Parameter Identification
 - Methods
 - Results and Discussion
- Development of Physical System
 - Methods
 - Results and Discussion
- Conclusion

Introduction



Introduction

- Cardiovascular diseases are one of the major causes of death all over the world [1]
- In such a case, it is very important to develop new and improved diagnostic and therapeutic methods and devices for the cardiovascular system.
- Modeling the cardiovascular system attempts to increase our understanding of its functions and processes.
- Due to complexity of system and data collection, modelling the complete distributed system is not feasible.
- CFD studies of the cardiovascular system is a powerful tool to aid in modelling of cardiovascular devices [2]
- But it requires proper boundary conditions
- So, to test the physical system, similar boundary condition/ load must be simulated
- Input impedance is a good choice of the boundary conditions and also to act as a load on the heart [2]



Goal

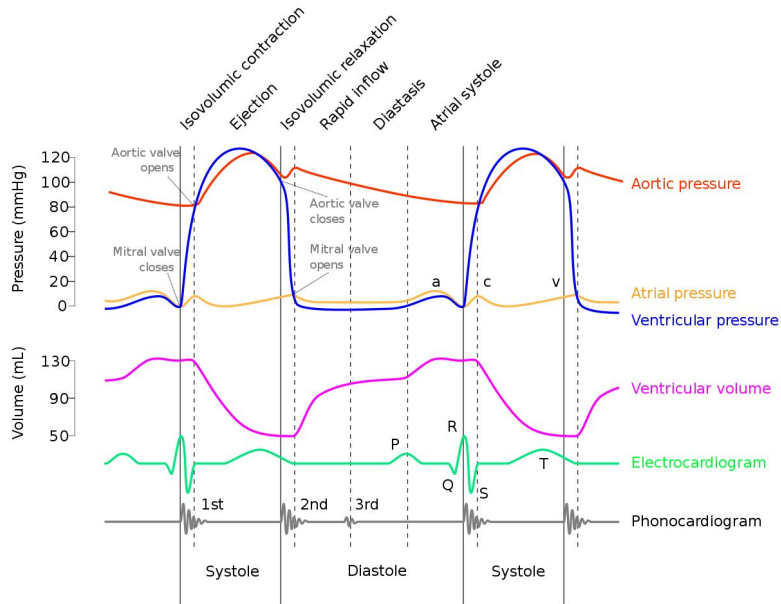
Design a physical module to simulate the input impedance of the systemic arterial circulation

Objectives

- Model selection
- Identification of parameters
- Convert the mathematical model into a physical model

Introduction

The Arterial Load



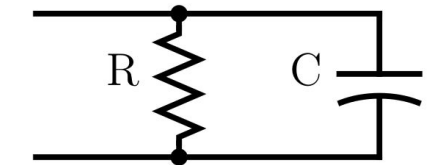
- Initial clinical study used resistance as the arterial load
- Later, found the pulse pressure to be an indicator of cardiovascular morbidity
- So the impedance load must be able to:
 - Produce the mean flow properties
 - Produce the pulsatile characteristics

Introduction

The Lumped Representation of Impedance

- 1773- Hales recorded that the behaviour of arterial load is similar to air-dome of Fire-engine-*Windkessel*
- High pulsatility of ventricular output vs the relatively constant aortic flow suggests presence of compliance element
- Frank (1889) suggested a model that contained - one resistance unit (Obey Poiseuille's Law) and one compliance unit.
- The pressure was assumed to be same at all points- Lumped model.

$$Q = \frac{P}{R} + C \cdot \frac{dP}{dt}$$

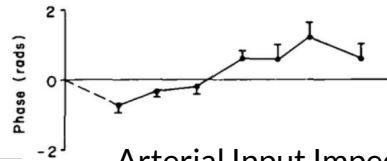
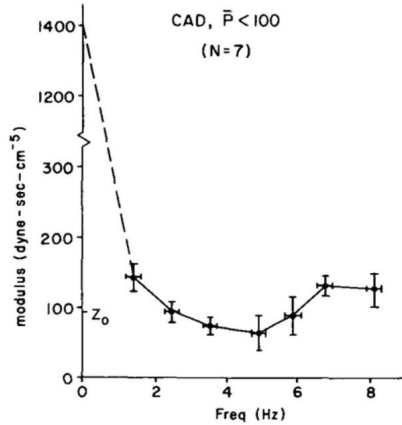


Two element Windkessel (WK)

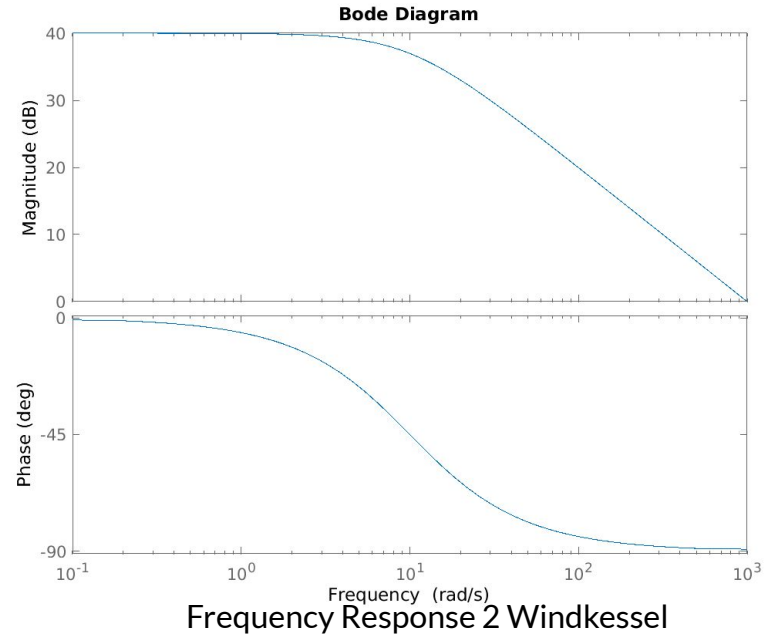
- It produces realistic physiological diastolic characteristics

Model Selection

Characteristic Impedance



Arterial Input Impedance [3]



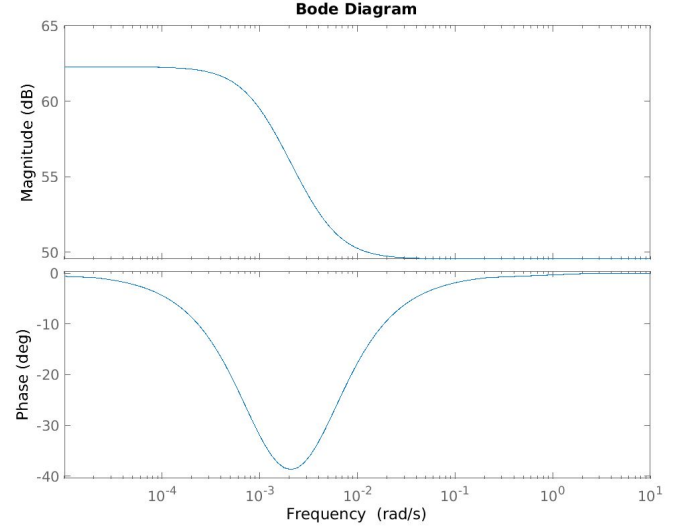
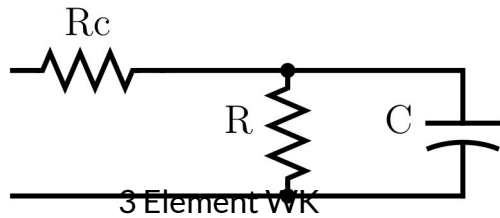
Model Selection

Characteristic Impedance

- Wave Propagation is not represented by a lumped model
- But the impedance saturates at characteristic impedance
- Wave reflection Coefficient:
- At high frequency, reflection wave is damped

$$\tau = \frac{Z_c - Z_{in}}{Z_c + Z_{in}}$$

- Introduce a new element - Characteristic 'Resistance'
-

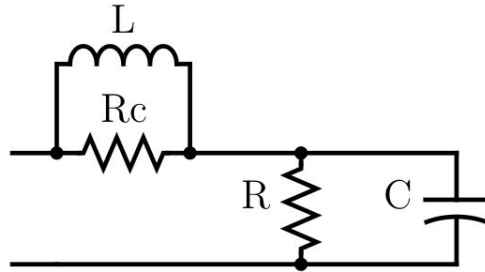


Frequency Response 3 WK

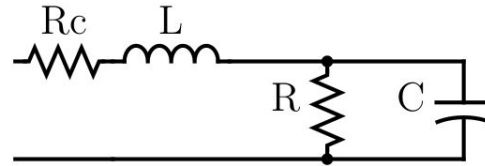
Model Selection

Inductance

- The introduction of new resistance introduces error at low frequencies [4]
- Low frequency motion should be influenced by inertia of blood [5]
- But inertia term is missing from the design
- So, introduce a inertia term -inductance



(a) WK4p Model

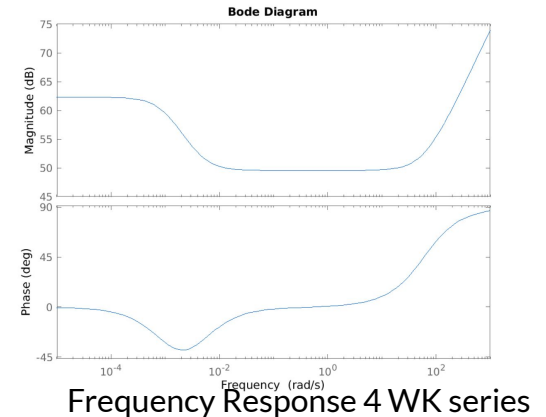
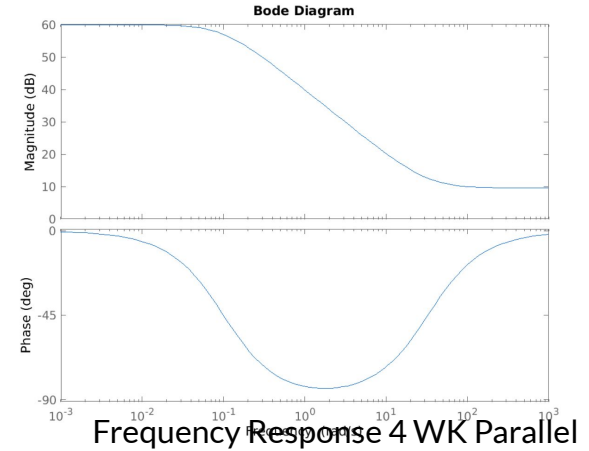


(b) WK4s Model

Model Selection

The Final Model Selection

- Both parallel and serial models have been used in previous research
- So, we need to make a choice between the two
- One study justified the use of parallel model using the similarity in the frequency response [5]
- But recently, it was found that the value of inductance in the series model could more closely explain the inertia of the blood [6]
- Moreover, we need the model to directly map to a corresponding hydraulic element
- So, we select the the series configuration



Identification of Parameters



Introduction

- After selecting the model, we can use it to determine the required design parameters.
- The L, C, R and R_c were used as design parameters to be optimized (with necessary constraints)
- The parameter estimation can be done based on a measured signal in response to a certain input.
- We use aortic flow rate as input and aortic pressure as the measured signal.
- A Fourier analysis can be implemented to determine the impedance at different frequencies.
- The optimization was done using the Impedance Method.

Identification of Parameters



Method

- The Parameter Estimation tool in Simulink Design Optimization™ toolbox is used to optimize the parameters values.
- We provided frequency as the input to the design tool and observed magnitude and phase of the impedance as the output.
- We use the nonlinear least square optimization method in the parameter estimation tool.
- After identifying parameters, we validated it with the reference data source.

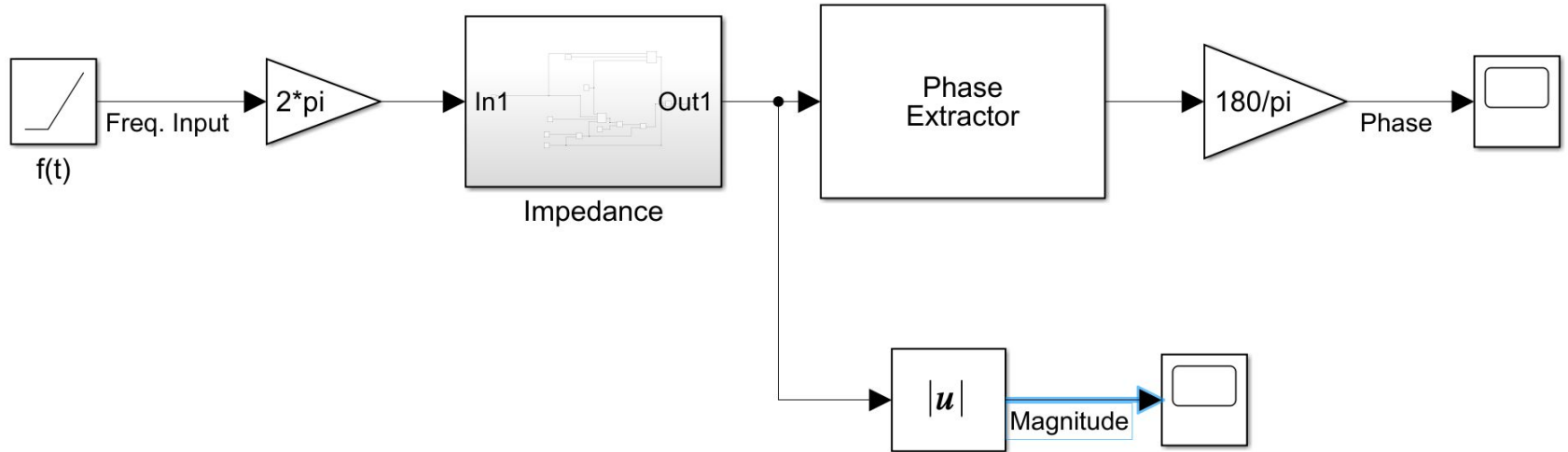
$$time, t_i = (0, 1, 2, \dots, 10)$$

$$\implies frequency, f(t_i) = (0, 2.54, \dots, 25.4)$$

$$\implies impedance, Z = Z(f(t_i))$$

Identification of Parameters

Method



Impedance System in Simulink

Identification of Parameters

Method: Inputs

- The clinical data was obtained from the literature: 'Aortic input impedance in infants and children'. [We did not collect clinical data by ourselves] [7]

Age Yr.	Heart Rate beats/min.	Mean Pressure mmHg	Systolic Pressure mmHg	Diastolic Pressure mmHg	Mean FLOW L/min
1.1	152.4	55.17	62.07	47.37	1.42

Frequency (Hz)	0	2.5	5	7.5	10	12.5	15	17.5	20	22.5	25
Magnitude	3125.9	448.66	340.7	492.55	450.52	906.79	574.12	456.4	570.8	546.01	434.76
Phase	0	225.71	5.64	23.14	33.82	26.5	27.56	14.03	16.24	34.98	25.55

Identification of Parameters



Method: Initial value Calculation

- The total peripheral resistance (TPR) can be determined from the 0 frequency impedance value. In case of WK4S, the TPR corresponds to $R_c + R$.
- At higher frequencies (2-8 Hz), the magnitude of impedance will remain close to R_c .
- The characteristic impedance can be estimated by using the averaged impedance magnitudes at higher harmonics.
- Compliance, C , can be estimated as the ratio of stroke volume to pulse pressure.
- The initial value inductance is approximated by taking in consideration the order of impedance values at higher harmonics.

Identification of Parameters

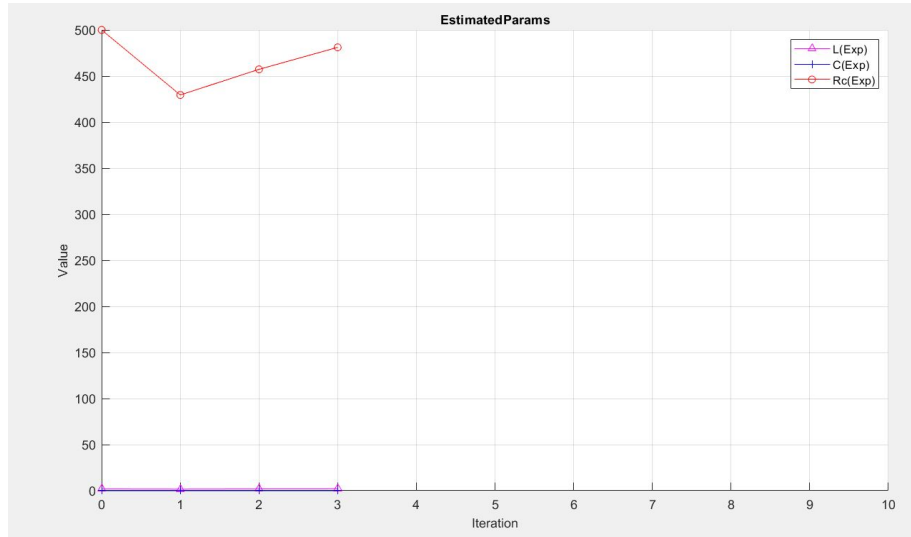


Method: Initial Values of the Model

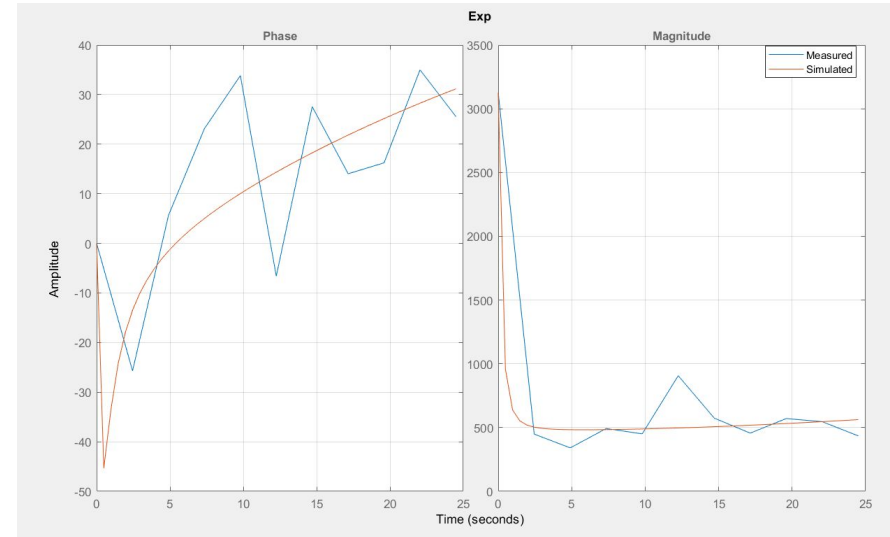
- $R + R_c = 3125.9 \text{ dyn.s.cm}^{-5}$
- $R_c = 502 \text{ dyn.s.cm}^{-5}$
- $C = 0.001 \text{ cm}^5/\text{dyn}$
- $L = 1 \text{ dyn.cm}^{-5}.\text{s}^2$

Identification of Parameters

Results:



Convergence of estimated Parameters



Optimized Fit

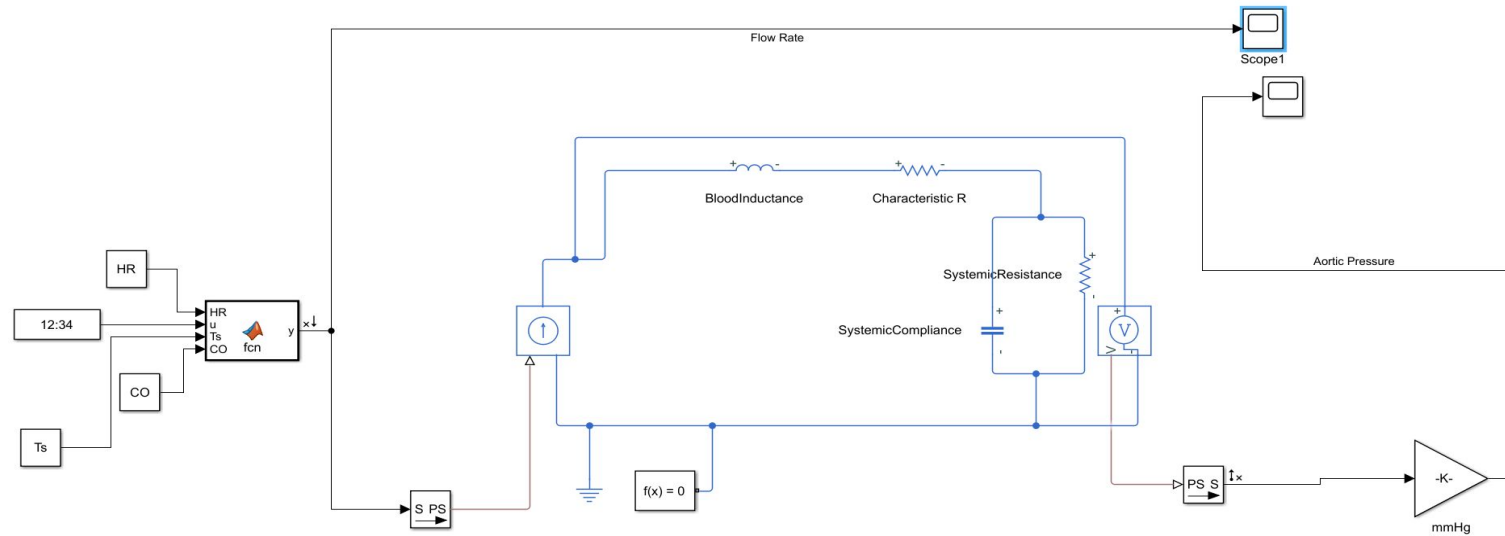
Identification of Parameters

Results: Optimized Parameters

Parameters	Optimized	Validation	Difference %
$R+R_c$ (dyn.s.cm ⁻⁵)	3125.9	3125.9	0
R_c (dyn.s.cm ⁻⁵)	481.75	480	0.36
C (cm ⁵ /dyn)	4.23e-4	4.9e-4	13.6
L (dyn.cm ⁻⁵ .s ²)	1.92	1.7	12.9

Identification of Parameters

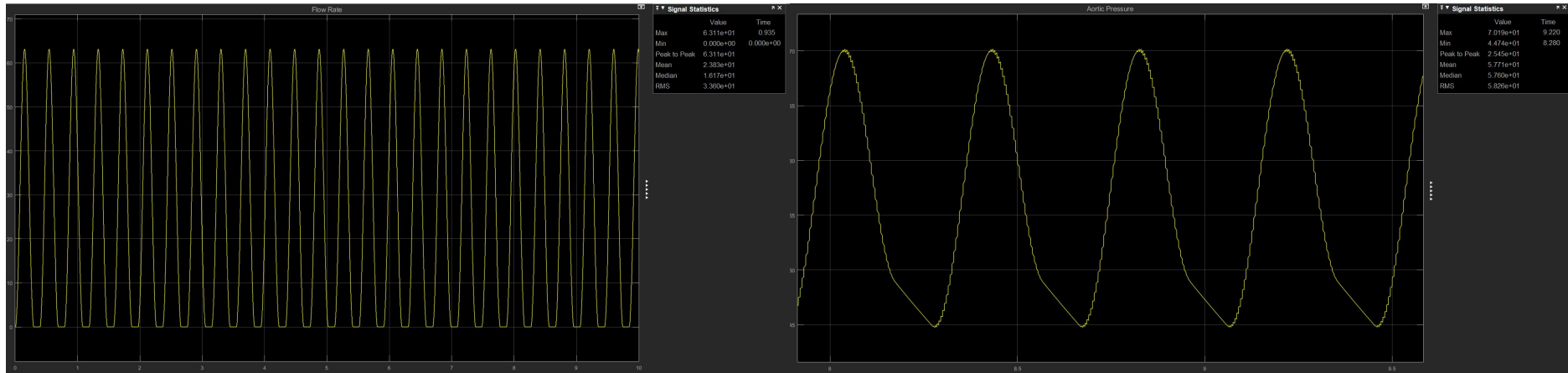
Validation (Alternative)



The circuit representation of WK4s in Simscape



Validation (Alternative)



Input flow and Output AoP

Physical Model



Introduction

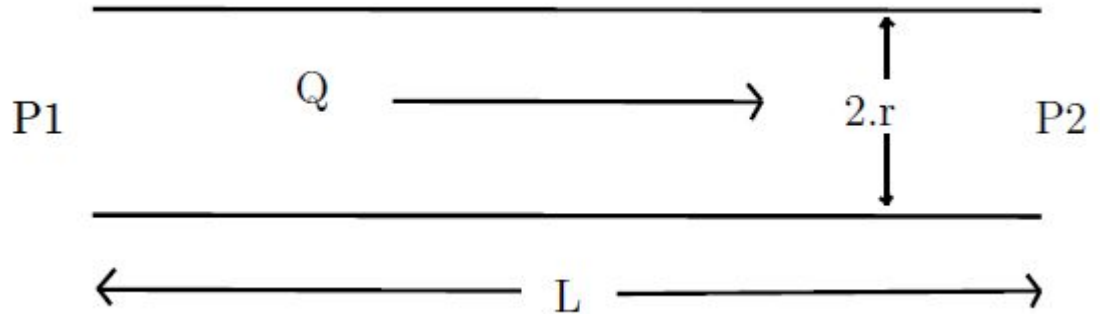
- We use the parameters optimized before to build a physical model for the windkessel.
- We need to identify the corresponding elements in the hydraulic circuit.
- We consider a 40 % glycerol solution is considered to be the fluid due to its similar dynamic viscosity with blood.

Physical Model

Resistance

- When a fluid flows through a pipe, there is a drop in pressure across the any two points along the direction of the flow.
- Where,

$$R = \frac{\Delta P}{Q} = \frac{8\mu L}{\pi r^4}$$





Inductance

- The inductance represents the inertia of the fluid.
- It is a measure of the the force required to accelerate the blood.
- The inductance, L is described by:

$$\Delta P = L \cdot \frac{dQ}{dt}$$

- For a conduit of cross-sectional area A and length l in which fluid of density ρ is flowing, the inductance will be:

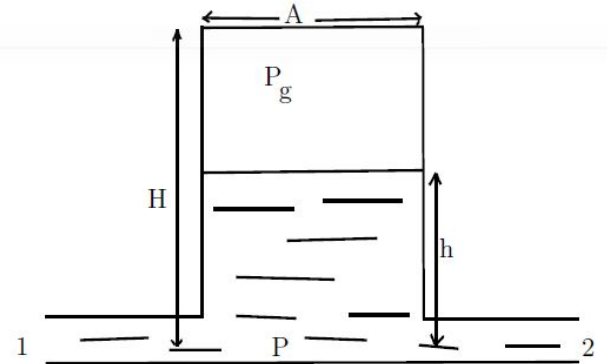
$$L = \frac{\rho \cdot l}{A}$$

Physical Model

Compliance

- Compliance in its literal sense means change in volume due to applied load or pressure.
- For a system shown, compliance can be represented as,

$$C = \frac{V}{P_g} = \frac{A.(H - h)}{P_g} = \frac{A.(H - h)}{P - \rho.g.h}$$



Physical Model



Methods

- To achieve the flow rate through a given cross sectional area pipe, Kung et al. [1] showed that parallel resistors can be used to create the resistance required.
- Kung showed that a nearly constant resistance can be built using capillary tubes packed in a cylinder. It also ensures ensures that the flow is laminar which is necessary to apply Poiseuille's Law.
- The total Resistance of the system is given by :

$$\text{Total Resistance, } R_{total} = \frac{8\mu l}{N\pi r^4} = \frac{8\mu l}{A \cdot r^2}$$

Where, N is the number of capillary tubes and r is the inner radius of the capillary tubes



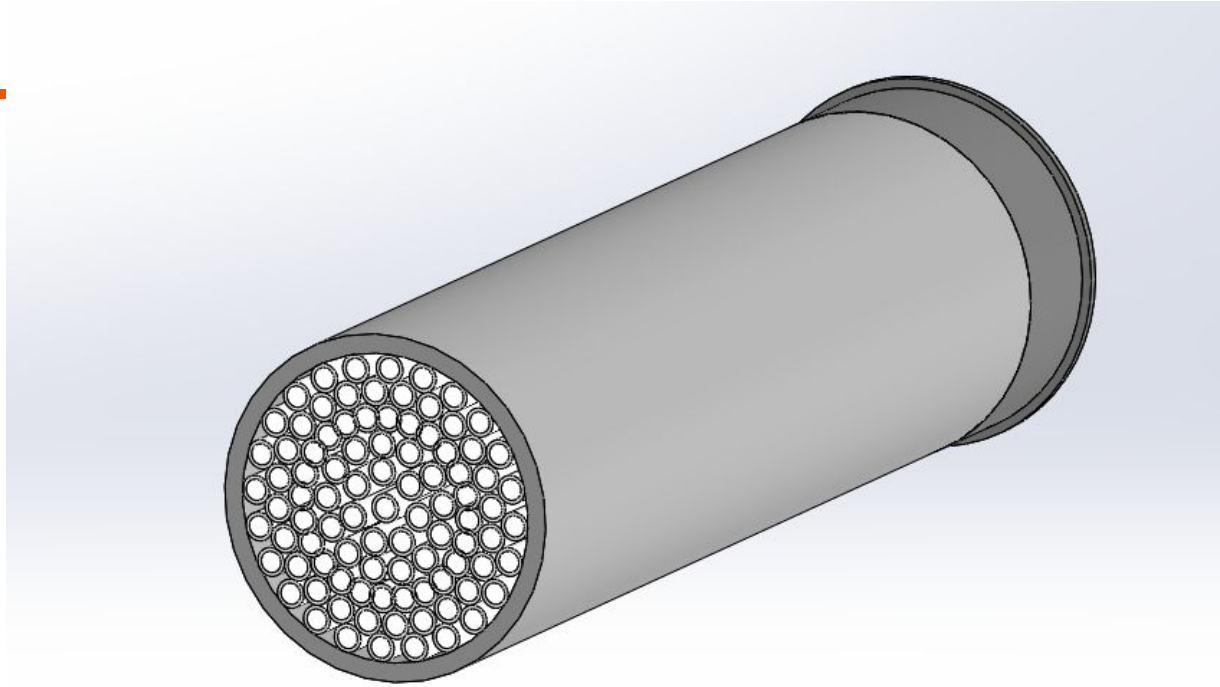
Methods

- We want to introduce inductance in the model
- The Compliance, due to its large cross section would have low inductance
- So, the inductance of the downstream components can be ignored
- We assign the inductance to the characteristic resistance, R_c module

$$R_{total} = \frac{8\mu L}{\rho r^2}$$

- For the compliance chamber, height is calculated for a compliance value and mean fluid pressure
- The air pressure is then adjusted to maintain the pressure of liquid in the circuit.

Physical Model



Capillary tube packed resistance module

Physical Model



Results

- By following the methods, we get the following dimensions for the setup.
- For the characteristic resistance, R_c with inductance, L incorporated in it:
 - Inner radius of capillary tubes: 0.31 mm
 - Length of capillary tubes: 10 cm (standard length)
 - Number of capillary tubes: 1882
 - Radius (inner) of the cylinder of pack the capillary tubes: 23.2 mm (assuming capillary OD=1mm)

Physical Model



Results

- For the other resistance, R module:
 - Inner radius of capillary tubes: 0.24 mm
 - Length of capillary tubes: 10 cm (standard length)
 - Number of capillary tubes: 1000
 - Radius (inner) of the cylinder of pack the capillary tubes: 17mm (assuming capillary OD=1mm)

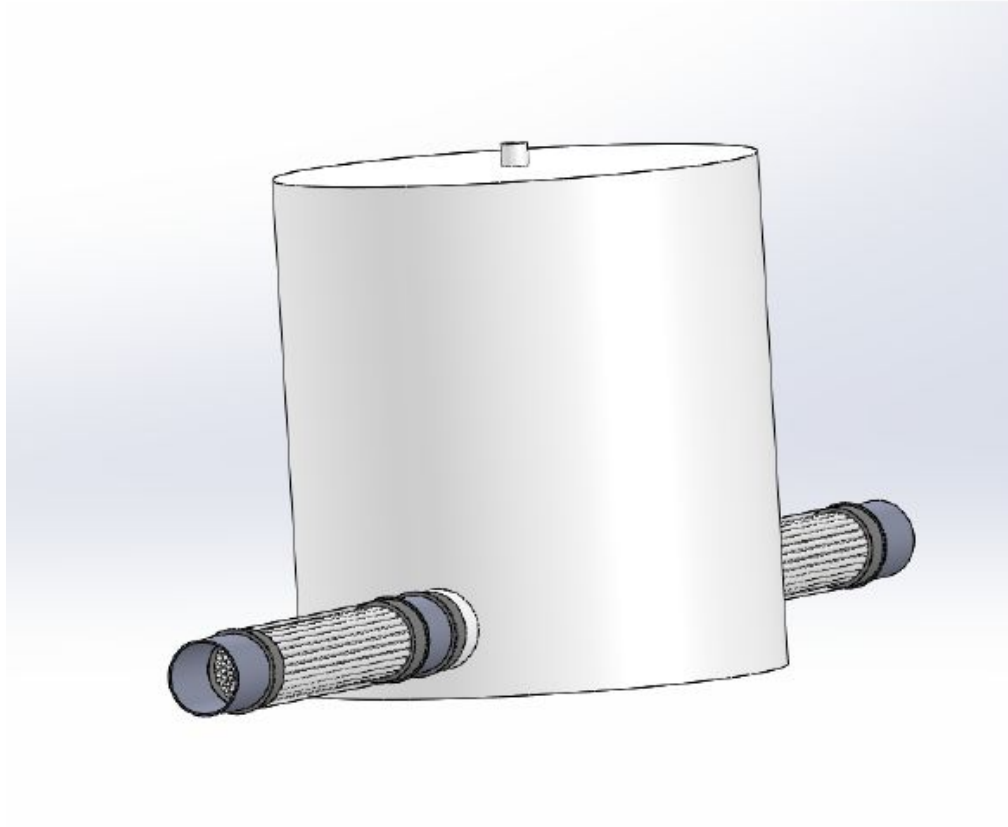
Physical Model



Results

- For the compliance, C module:
 - Inner radius of the cylindrical chamber: 10 cm
 - Height of the liquid column: 11.5 cm [Will change with mean pressure]
 - Total height of the cylinder: 25 cm
 - Pressure of air above the liquid: $60800 \text{ dyn.cm}^{-2}$ [Will change with change in mean pressure]

Physical Model



CAD representation of assembled system


Physical Model




Discussion

- Introduction of inductance in R_c increases its diameter
- Pumps may not be compatible with large diameter
- The diameter can be adjusted by using a non-standard shorter capillary tubes.
- Reduction in diameter will also reduce the sectional area of the other conduits and will add extra inductance to the circuit
- A conduit of gradually increasing diameter may be used
- The area of the compliance should always be large enough for assumptions to hold
- Laminar flow should be ensured for maximum flow rate in the circuit

Conclusion

- 
- We have used the modelling techniques to design a device that can act as the systemic arterial load.
 - The device, when fabricated can be used to test artificial valves or ventricular-assist devices.
 - The optimization analysis on the electrical model was used to finally design the mechanical (hydraulic) system.
 - We have been able to incorporate the inductance in the design.
 - Use of modelling tools like Simulink made the process easy and fast
 - We have used a single windkessel unit to model the systemic circulation only.
 - Similar approach can be used to model and design a system for the pulmonary circulation and cascaded windkessel models

References (For presentation only)

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- [1]. A. Gaziano, Cardiovascular disease in the developing world and its cost-effective management, *Circulation* 112 (23) (2005) 3547–3553.
- [2]. E. O. Kung, C. A. Taylor, Development of a physical windkessel module to re-create in vivo vascular flow impedance for in vitro experiments, *Cardiovascular engineering and technology* 2 (1) (2011) 2–14.
- [3]. W. Nichols, C. R. Conti, W. E. Walker, W. R. Milnor, Input impedance of the systemic circulation in man., *Circulation research* 40 (5) (1977) 451–458.
- [4]. N. Westerhof, J.-W. Lankhaar, B. E. Westerhof, The arterial windkessel, *Medical & biological engineering & computing* 47 (2) (2009) 131–141.
- [5]. N. Stergiopoulos, B. E. Westerhof, N. Westerhof, Total arterial inertance as the fourth element of the windkessel model, *American Journal of Physiology-Heart and Circulatory Physiology* 276 (1) (1999) H81–H88.
- [6]. R. Burattini, P. O. Di Salvia, Development of systemic arterial mechanical properties from infancy to adulthood interpreted by four-element windkessel models, *Journal of Applied Physiology* 103 (1) (2007) 66–79.
- [7]. M. K. Sharp, G. M. Pantalos, L. Minich, L. Y. Tani, E. C. McGough, J. A. Hawkins, Aortic input impedance in infants and children, *Journal of applied physiology* 88 (6) (2000) 2227–2239.